

# Shape and Topology Optimization of Plane Frame Structure Using Force Density Method

**Wei Shen, Makoto Ohsaki**  
**Kyoto University, Japan**

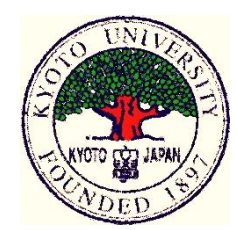


京都大学

KYOTO UNIVERSITY

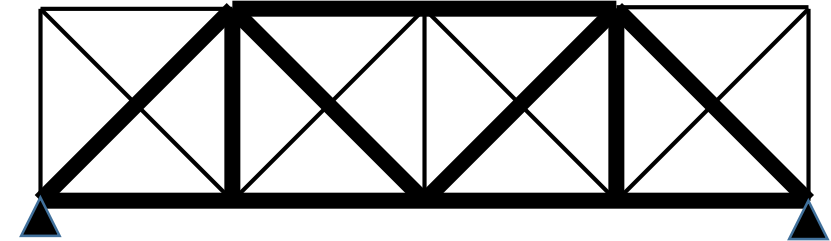
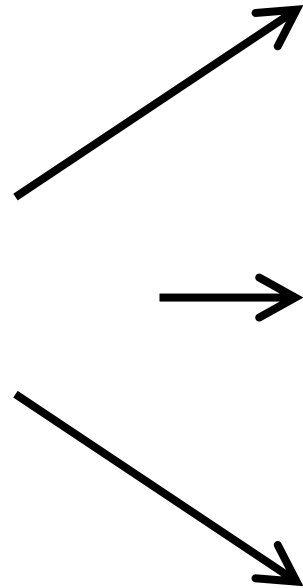
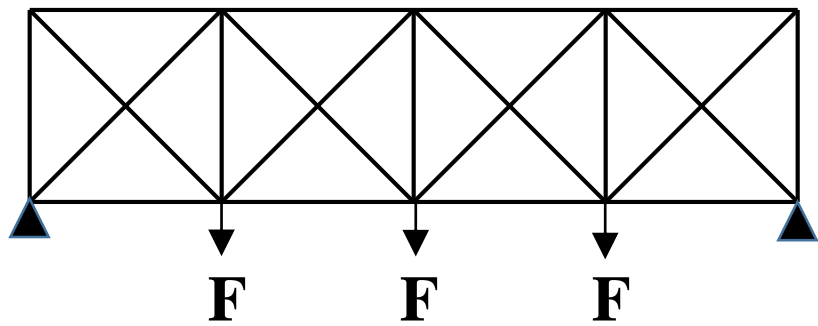
**Date : 2019.05.21**

**Reporter : Wei Shen**

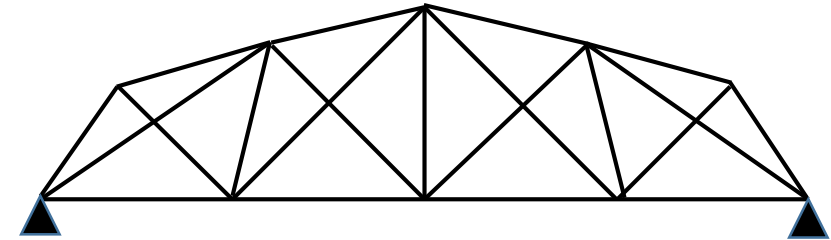


# *Optimization of Frames*

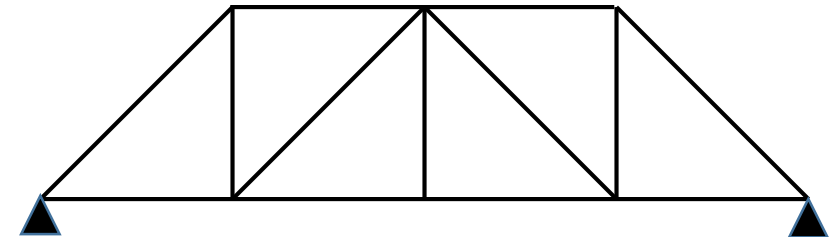
**Size Optimization**

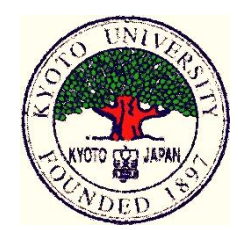


**Shape Optimization**



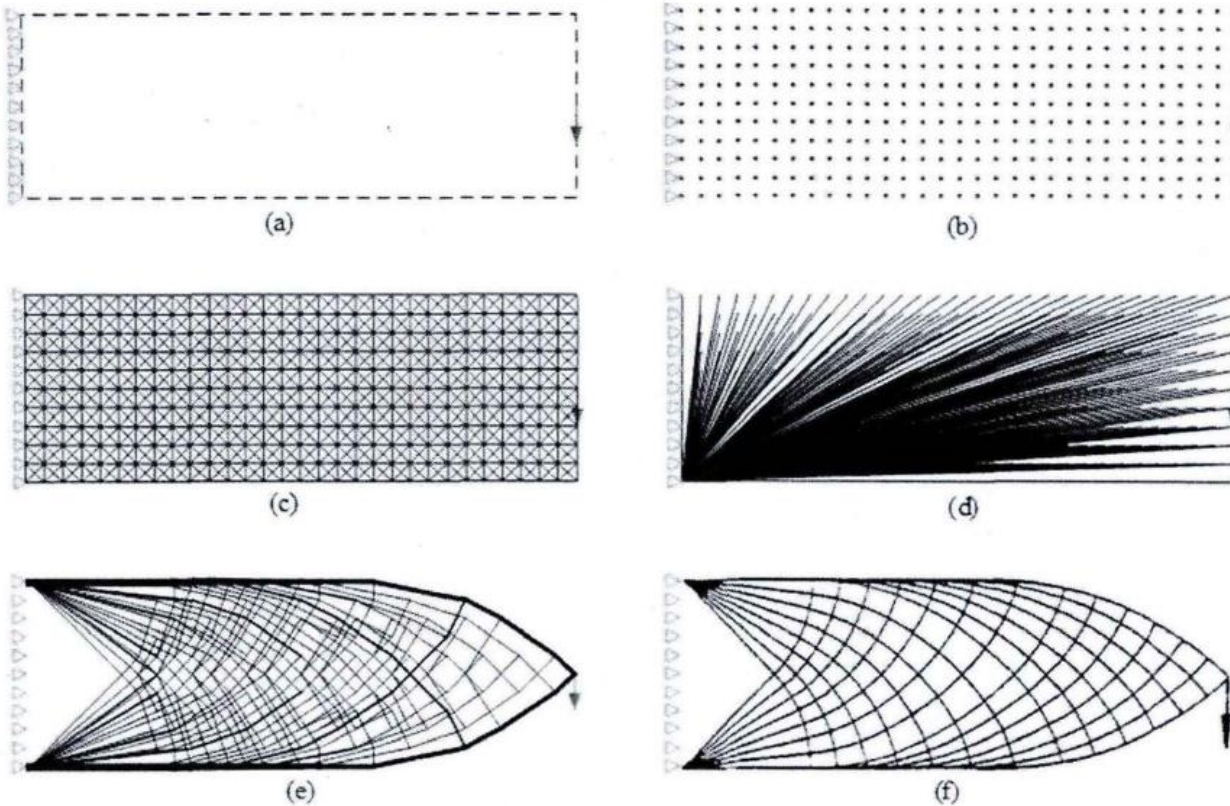
**Topology Optimization**



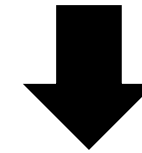


# Characteristics 1

- **Ground structure method**



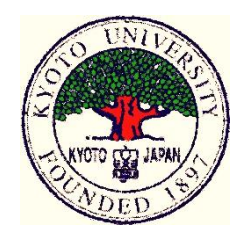
**Topology optimization**



**Size optimization**

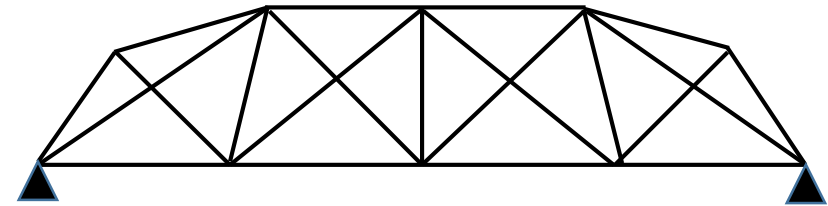
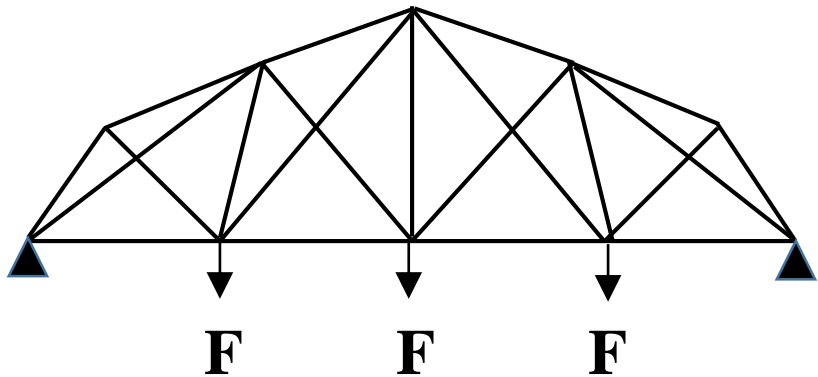
**Challenge: Influence of initial nodes and elements**

Source: Ge Gao, Research on theory and application of truss structure, 2016, PhD Thesis.



# *Possible approach*

- **Simultaneous Optimization**

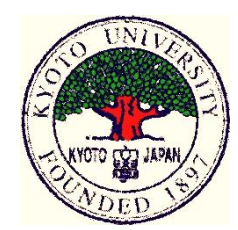


**Simultaneous optimization of shape and topology**

**Location of Nodes**

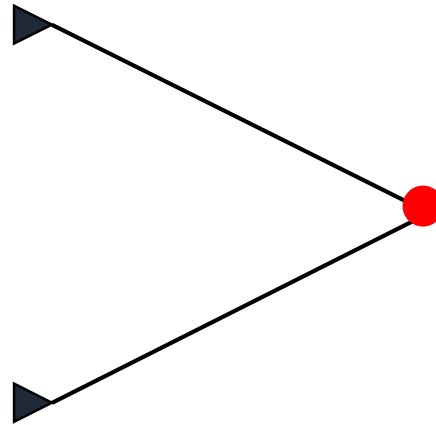
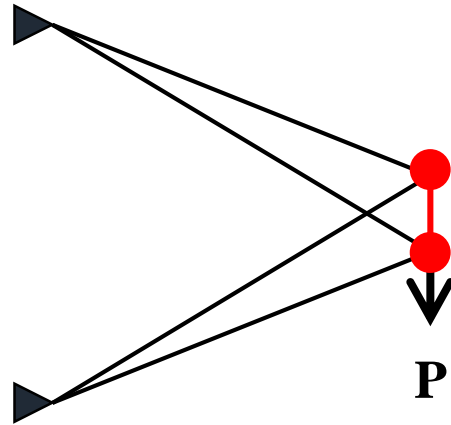
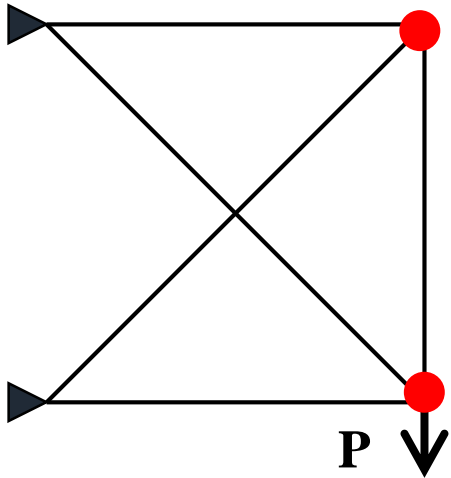


**Cross-section area  
of element**



# Characteristics 2

- **Melting nodes**



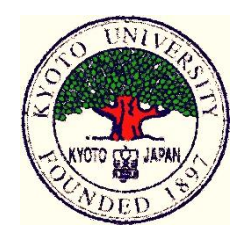
Stiffness Matrix



**Red nodes**  
get close

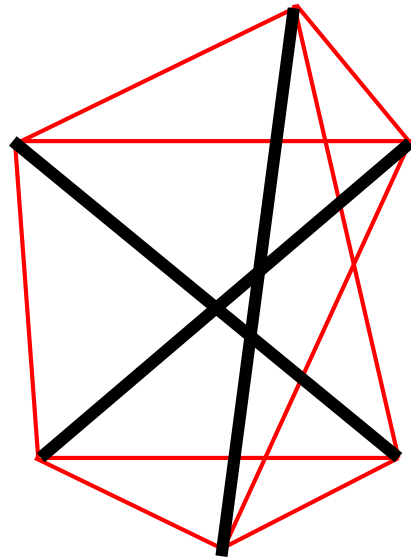
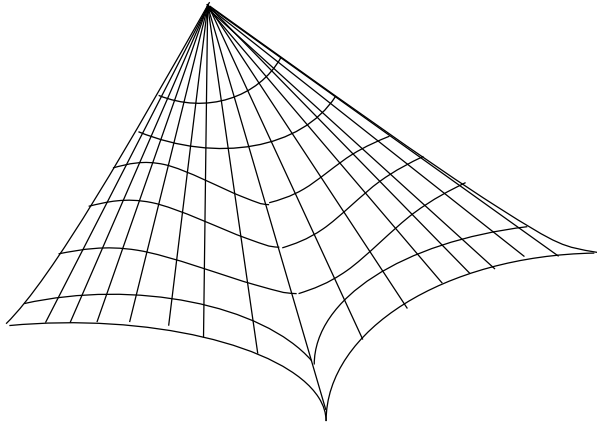
Singular

Desirable to avoid existence of extremely **short member**



# Possible approach

- Force density method(FDM)



Widely used in **tension** and **tensegrity** structure

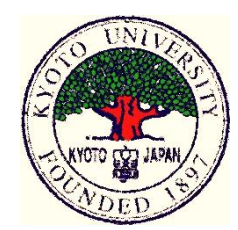
Force density  $q = \frac{N}{L}$     Axial force  
Member length

**$q$  for each element**

**Determine**

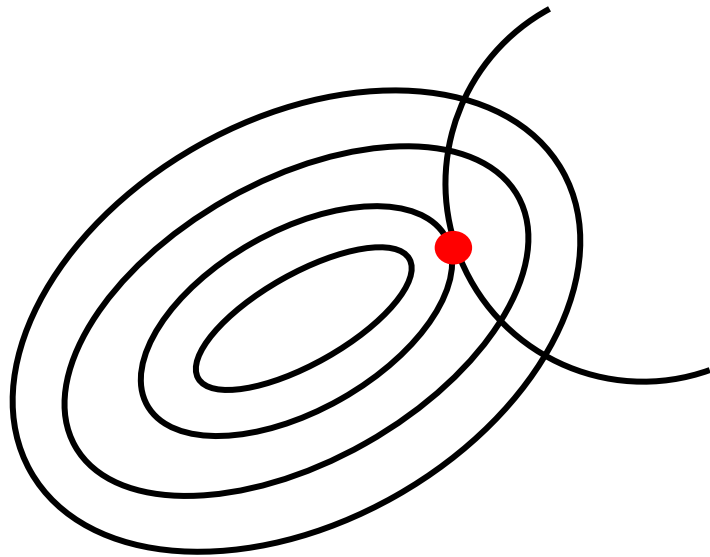


**Structural Shape**



# Characteristic 3

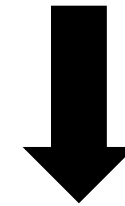
- **Nonlinear Programming**



$$\begin{aligned} &\text{Min } f(\mathbf{x}) \\ &s.t. \ h(\mathbf{x}) = \mathbf{0} \\ &\quad g(\mathbf{x}) \leq \mathbf{0} \end{aligned}$$

Shape optimization → Nodal location

**Nonlinear**

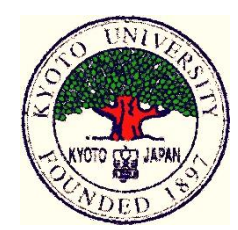


Structure Stiffness Matrix

**Sensitivity analysis**



Sequential quadratic programming (SQP)

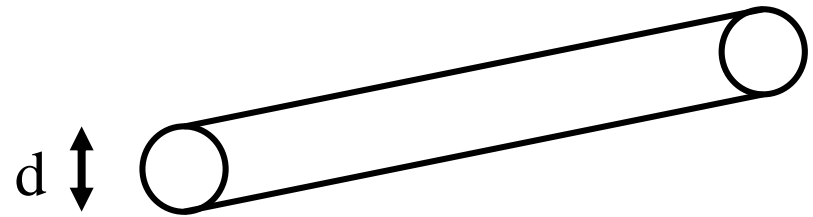


# *Problem Formulation*

*Minimize* :  $U^T K U$

*Subject to*:  $V \leq V_{upper}$

**Euler-Bernoulli beam element**

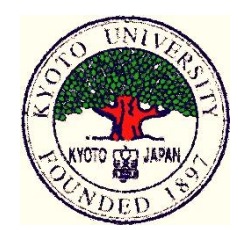


*Minimize* :  $U^T (X, Y, d) K (X, Y, d) U (X, Y, d)$

*Subject to*:  $V (X, Y, d) \leq V_{upper} (X, Y, d), d_{lower} \leq d \leq d_{upper},$

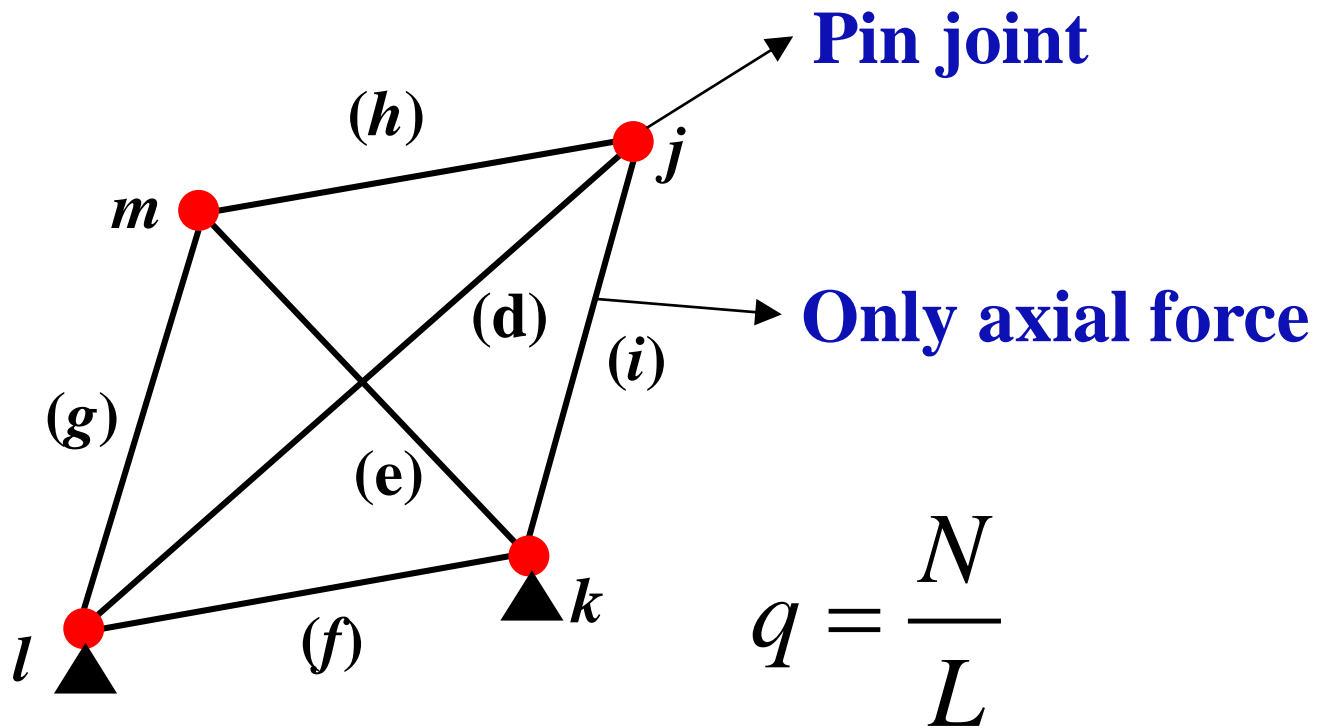
$X_{lower} \leq X \leq X_{upper}, Y_{lower} \leq Y \leq Y_{upper}$





# Introducing FDM

## Truss structure



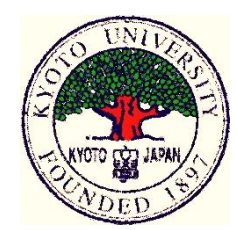
Shape optimization:  
**optimal nodal location**



**Only force equilibrium**

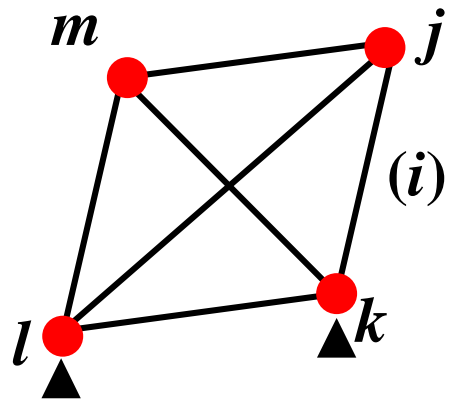


**Determined by  $q$**



# Introducing FDM

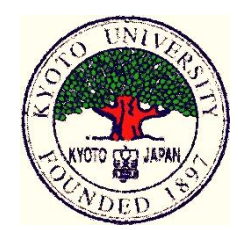
Denote the connectivity matrix as  $C$ , where



$$C_{(i,p)} = \begin{cases} 1 & p = j \\ -1 & p = k \\ 0 & \text{other case} \end{cases} \quad i=1,2, \dots, m; \quad j, k=1, 2, \dots, n$$

Divide nodes to **free** and **fix** nodes  
And rearrange the matrix  $C$

$$C = \begin{bmatrix} \underbrace{C_{1,1} \dots C_{1,n_{free}}}_{C_{\text{free}}} & \dots & \underbrace{C_{1,n_{fix}} \dots C_{1,n}}_{C_{\text{fix}}} \\ \vdots & \ddots & \vdots \\ \vdots & & \vdots \\ \vdots & & \vdots \\ C_{m,1} & \dots & C_{m,n} \end{bmatrix} = [C_{\text{free}} \quad C_{\text{fix}}]$$



# Introducing FDM

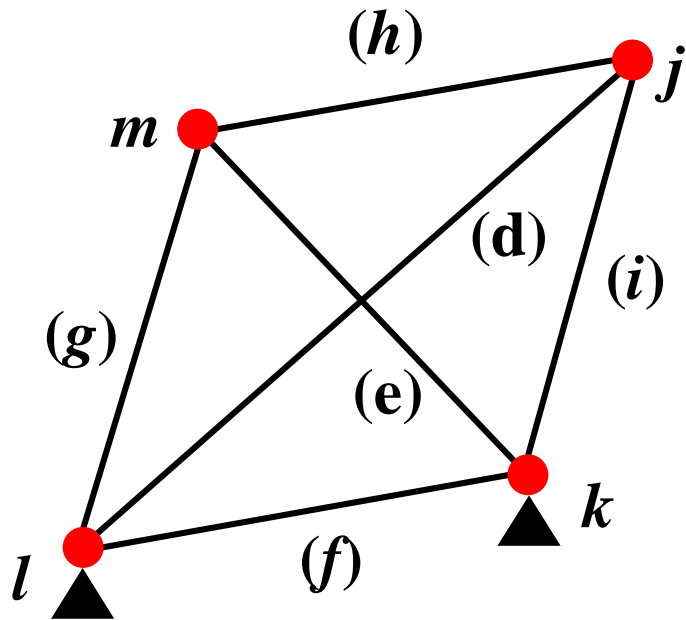
Denote the force density matrix as  $Q$ , where

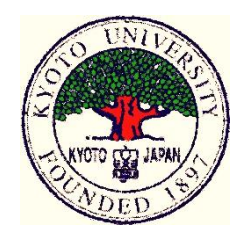
$$Q = (C_{\text{free}}, C_{\text{fix}})^T \text{diag}(q) (C_{\text{free}}, C_{\text{fix}}) = \begin{bmatrix} C_{\text{free}}^T \text{diag}(q) C_{\text{free}} & C_{\text{free}}^T \text{diag}(q) C_{\text{fix}} \\ C_{\text{fix}}^T \text{diag}(q) C_{\text{free}} & C_{\text{fix}}^T \text{diag}(q) C_{\text{fix}} \end{bmatrix}$$



Force density vector

$$q = (q_d, q_e, q_f, q_g, q_h, q_i)$$





# *Nodal location*

## Determination of nodal location

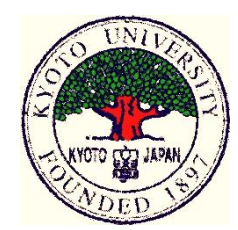
By introducing FDM, the location of free nodes can be derived from the following equation

$$\begin{aligned} C_{\text{free}}^T \text{diag}(q) C_{\text{free}} \mathbf{x}_{\text{free}} &= -C_{\text{free}}^T \text{diag}(q) C_{\text{fix}} \mathbf{x}_{\text{fix}} + P_{x,\text{free}} \\ C_{\text{free}}^T \text{diag}(q) C_{\text{free}} \mathbf{y}_{\text{free}} &= -C_{\text{free}}^T \text{diag}(q) C_{\text{fix}} \mathbf{y}_{\text{fix}} + P_{y,\text{free}} \end{aligned}$$

No external load on free nodes

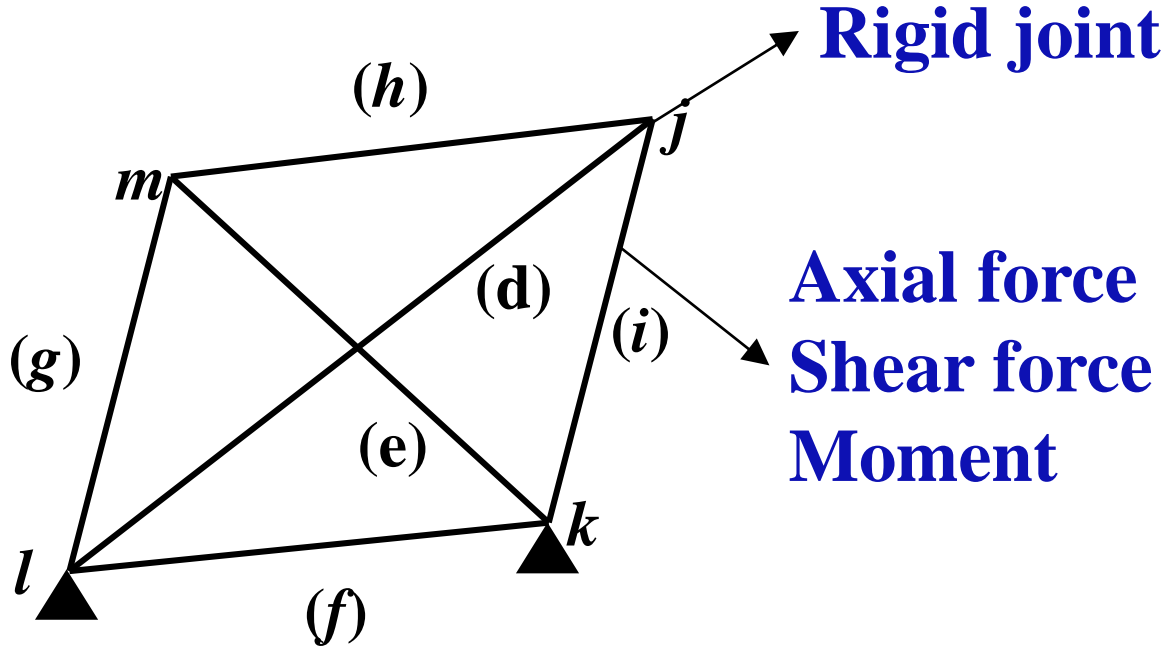
$$\begin{aligned} C_{\text{free}}^T \text{diag}(q) C_{\text{free}} \mathbf{x}_{\text{free}} &= -C_{\text{free}}^T \text{diag}(q) C_{\text{fix}} \mathbf{x}_{\text{fix}} \\ C_{\text{free}}^T \text{diag}(q) C_{\text{free}} \mathbf{y}_{\text{free}} &= -C_{\text{free}}^T \text{diag}(q) C_{\text{fix}} \mathbf{y}_{\text{fix}} \end{aligned}$$

Functions of  $q$



# Problem Reformulation

## Frame structure



Same discretization with **Truss**

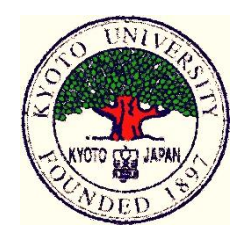
FDM ( $q$ )



Optimal shape of **Frame**

**Minimize :**  $U^T (X(q), Y(q), d) K (X(q), Y(q), d) U (X(q), Y(q), d)$

**Subject to:**  $V (X(q), Y(q), d) \leq V_{upper}, d_{lower} \leq d \leq d_{upper}, q_{lower} \leq q \leq q_{upper}$



# Sensitivity Analysis

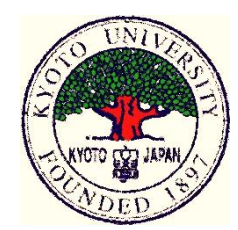
For objective function

$$\frac{\partial U^T K U}{\partial q_i} = \sum_{j=1}^n \boxed{\frac{\partial U^T K U}{\partial X_j}} \times \frac{\partial X_j}{\partial q_i} + \boxed{\frac{\partial U^T K U}{\partial Y_j}} \times \frac{\partial Y_j}{\partial q_i}; \quad \frac{\partial U^T K U}{\partial d_i} = U^T \frac{\partial K}{\partial d_i} U$$

$$\frac{\partial U^T K U}{\partial X_j} = U^T \frac{\partial K}{\partial X_j} U; \quad \frac{\partial U^T K U}{\partial Y_j} = U^T \frac{\partial K}{\partial Y_j} U;$$

**Adjoint variable method**

$\frac{\partial X_j}{\partial q_i}, \frac{\partial Y_j}{\partial q_i}$  : **Only free nodes are considered**



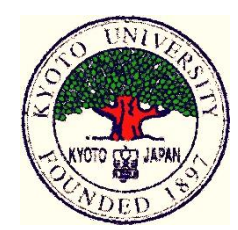
# *Sensitivity Analysis*

$$\frac{\partial X_{free}}{\partial q_i} = -\left(\mathbf{C}_{free}^T \mathbf{Q} \mathbf{C}_{free}\right)^{-1} \left( \frac{\partial \left(\mathbf{C}_{free}^T \mathbf{Q} \mathbf{C}_{free}\right)}{\partial q_i} X_{free} + \frac{\partial \left(\mathbf{C}_{free}^T \mathbf{Q} \mathbf{C}_{fix}\right)}{\partial q_i} X_{fix} \right)$$

$$\frac{\partial Y_{free}}{\partial q_i} = -\left(\mathbf{C}_{free}^T \mathbf{Q} \mathbf{C}_{free}\right)^{-1} \left( \frac{\partial \left(\mathbf{C}_{free}^T \mathbf{Q} \mathbf{C}_{free}\right)}{\partial q_i} Y_{free} + \frac{\partial \left(\mathbf{C}_{free}^T \mathbf{Q} \mathbf{C}_{fix}\right)}{\partial q_i} Y_{fix} \right)$$

## **For Volume constraint**

$$\frac{\partial V(X(\mathbf{q}), Y(\mathbf{q}), \mathbf{d})}{\partial q_i} = \sum_{i=1}^n A_i \left( \sum_{i_k=1}^s \frac{\partial L_i}{\partial X_{i_k}} \cdot \frac{\partial X_{i_k}}{\partial q_i} + \frac{\partial L_i}{\partial Y_{i_k}} \cdot \frac{\partial Y_{i_k}}{\partial q_i} \right); \quad \frac{\partial V(X(\mathbf{q}), Y(\mathbf{q}), \mathbf{d})}{\partial d_i} = \frac{\partial A_i}{\partial d_i} L_i$$



# Further Improvement

$$\text{Minimize : } U^T (X(q), Y(q), d) K (X(q), Y(q), d) U (X(q), Y(q), d)$$

$$\text{Subject to: } V (X(q), Y(q), d) \leq V_{upper}, d_{lower} \leq d \leq d_{upper}, q_{lower} \leq q \leq q_{upper}$$

Optimal result with **thin element** and **closely spaced nodes**

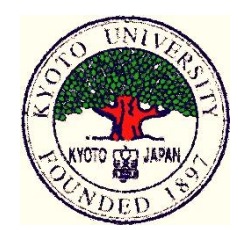


$$\text{Minimize : } U^T (X, Y, d) K (X, Y, d) U (X, Y, d)$$

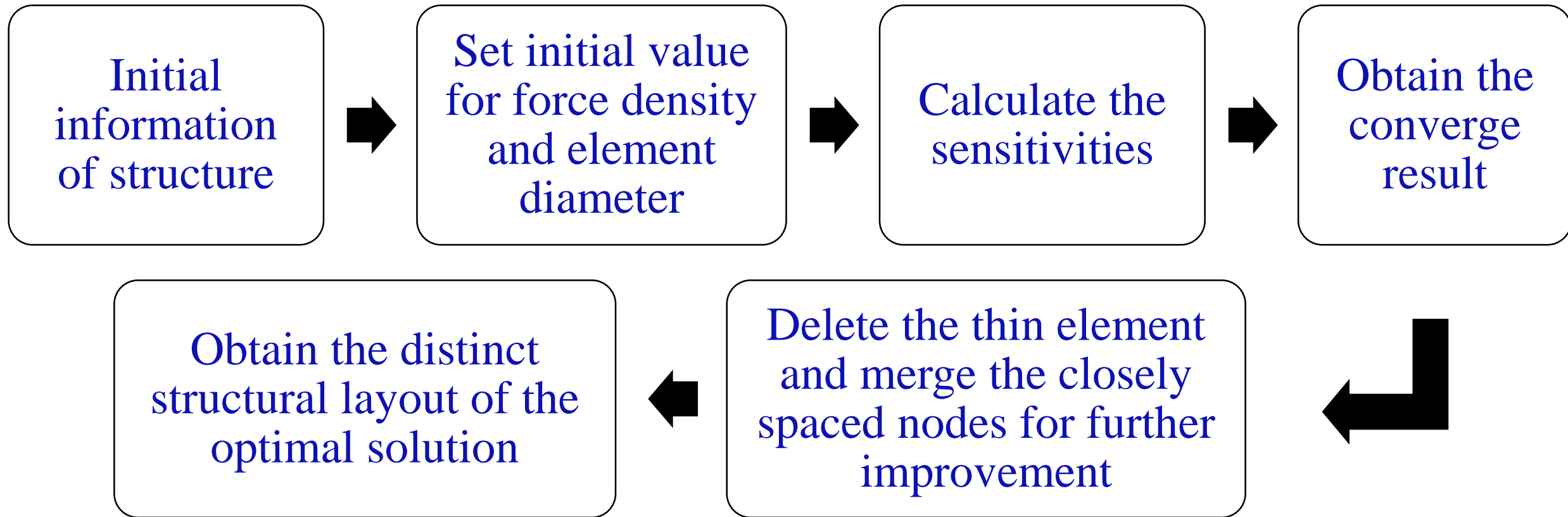
$$\text{Subject to: } V (X, Y, d) \leq V_{upper}, d_{lower} \leq d \leq d_{upper},$$

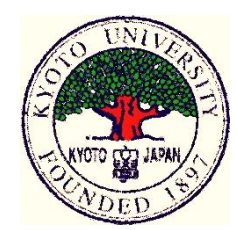
$$X_{lower} \leq X \leq X_{upper}, Y_{lower} \leq Y \leq Y_{upper}$$





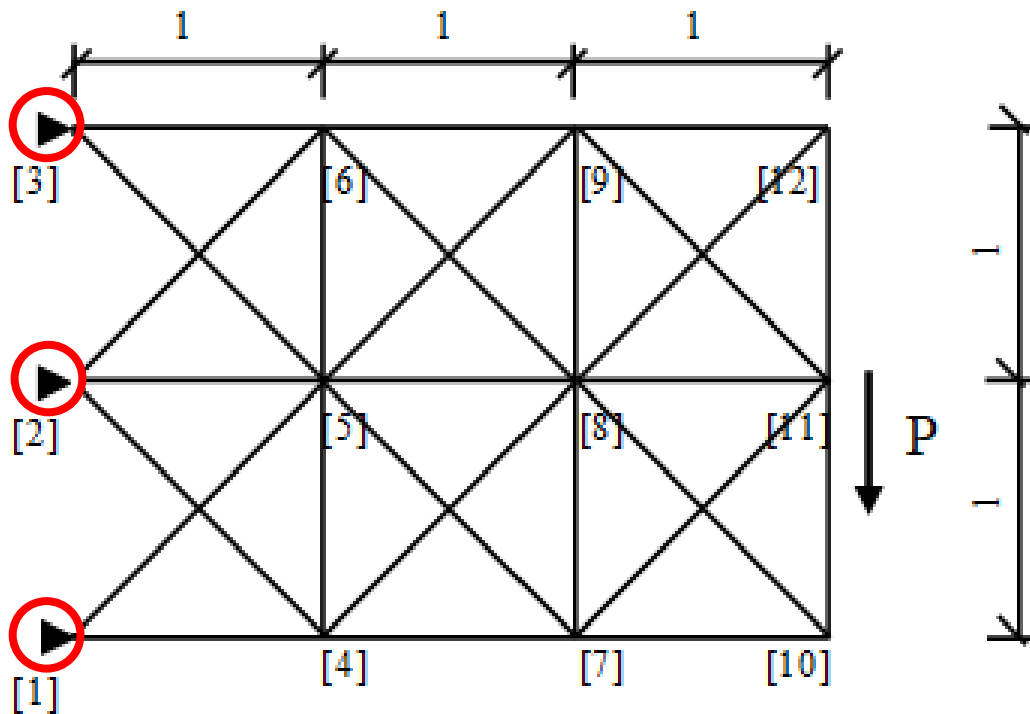
# *Flow chart*





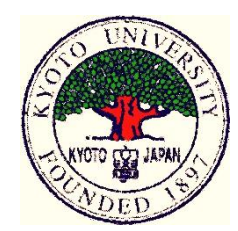
# Numerical Example 1

## ➤ Cantilever beam

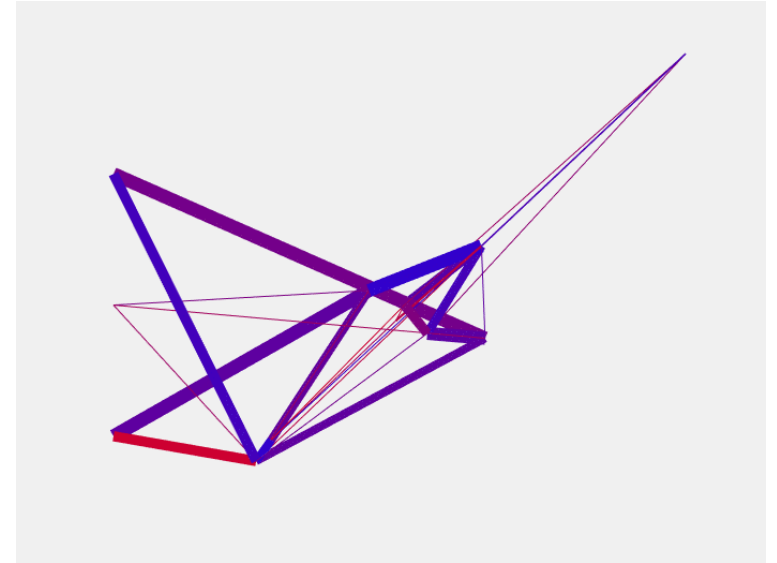
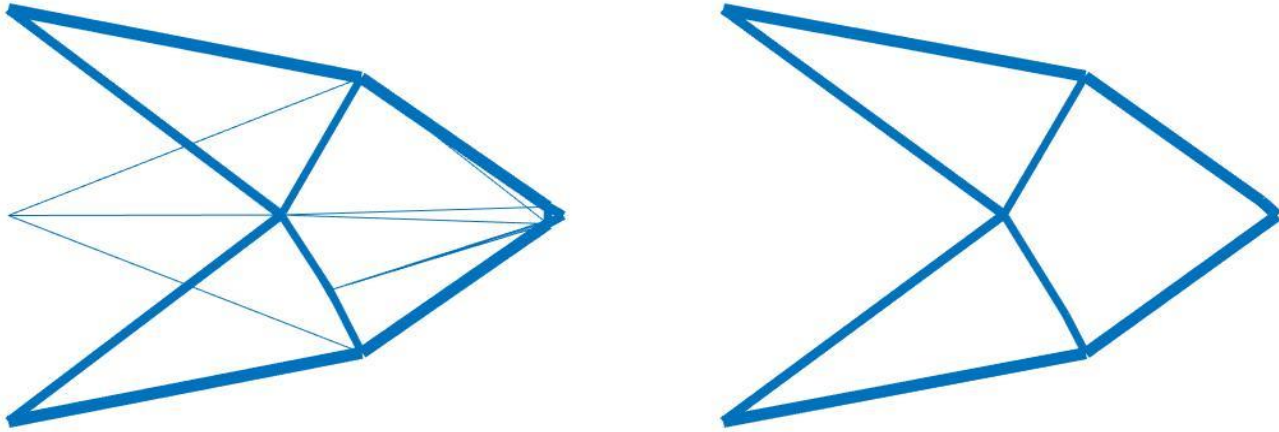


Pin support

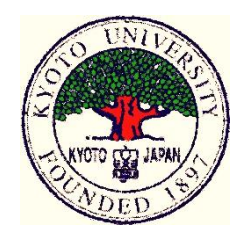
$$d_{\text{lower}} = 0.001 \text{ and } d_{\text{upper}} = \infty$$
$$q_{\text{lower}} = -1000 \text{ and } q_{\text{upper}} = 1000$$
$$V_{\text{upper}} = 1$$



# *Numerical Example 1*

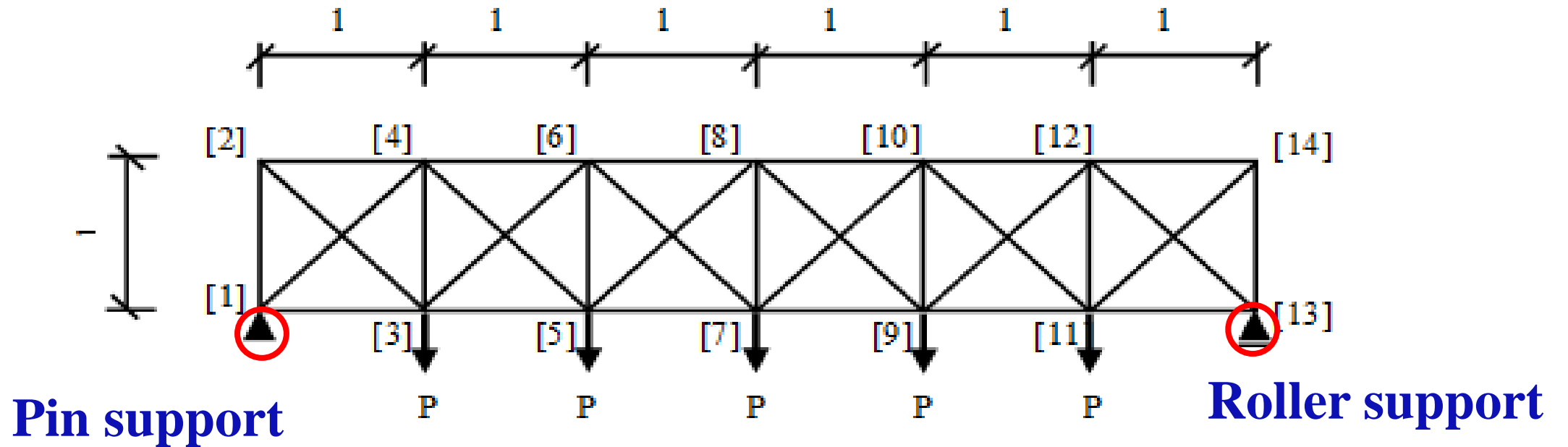


<b>Solution</b>	<b>Volume</b>	<b>Compliance</b>
Before	1	83.1183
After	1	82.0866

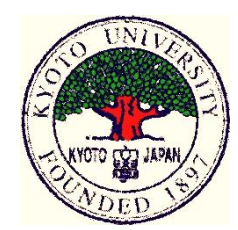


# Numerical Example 2

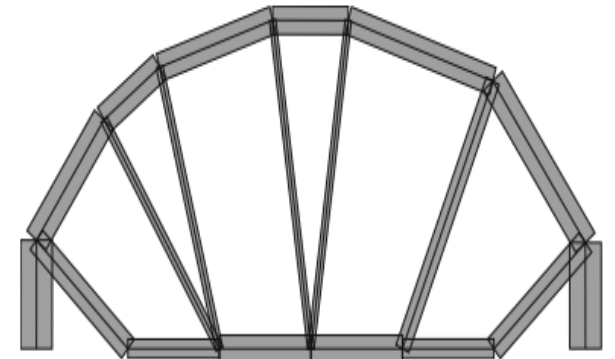
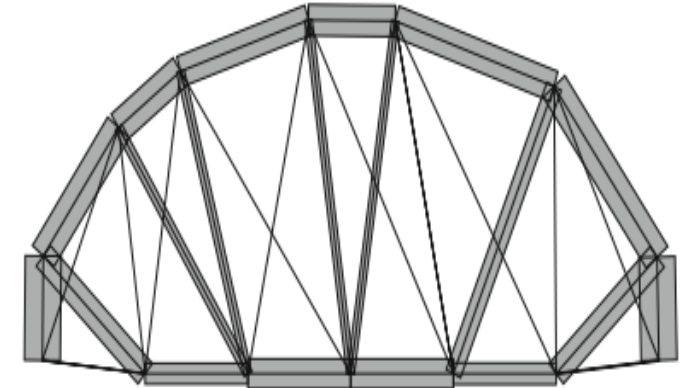
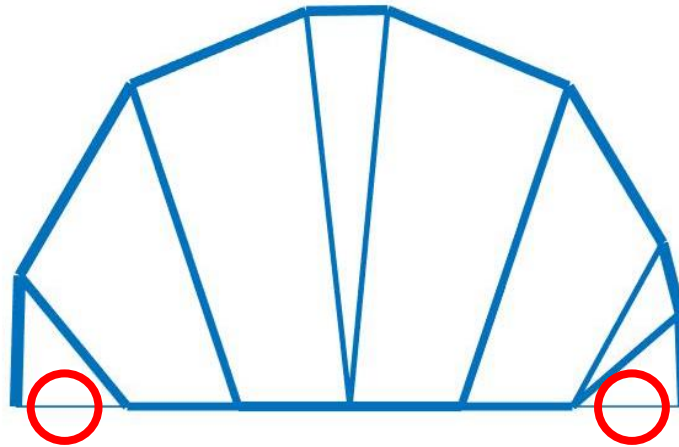
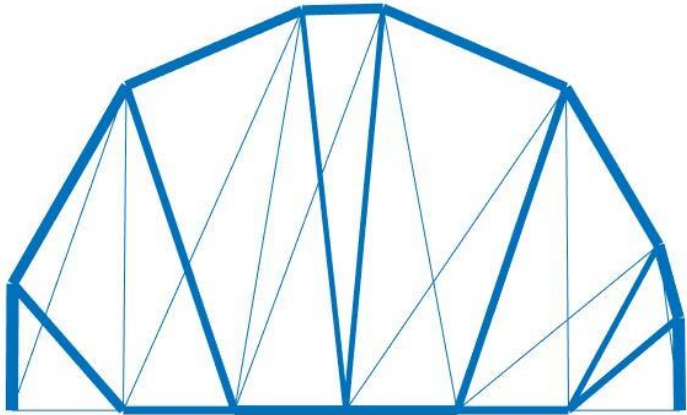
## ➤ Bridge beam



$$d_{\text{lower}} = 0.001 \text{ and } d_{\text{upper}} = \infty; q_{\text{lower}} = -1000 \text{ and } q_{\text{upper}} = 1000; V_{\text{upper}} = 1$$

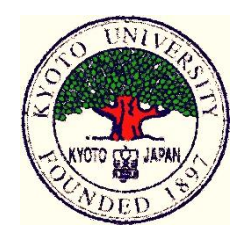


# Numerical Example 2

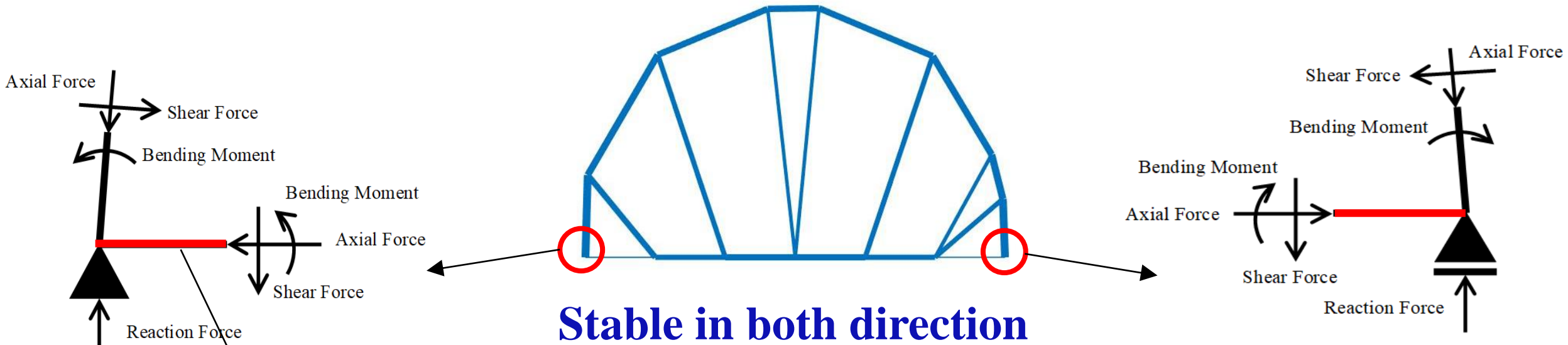


Solution	Volume	Compliance
Before	1	1221.0307
After	1	1219.2239

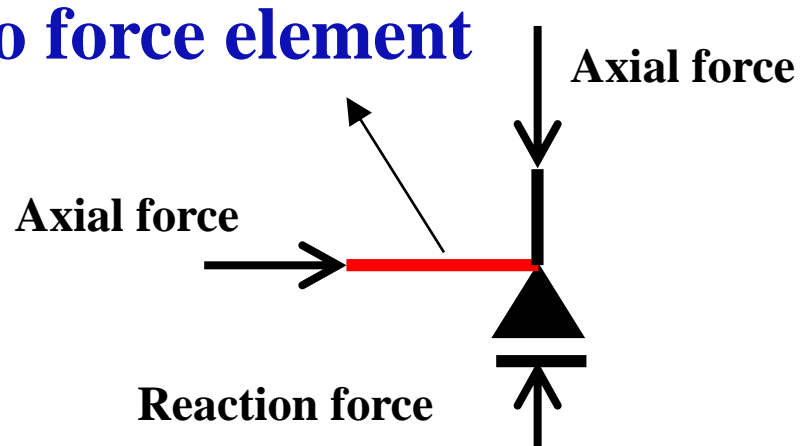
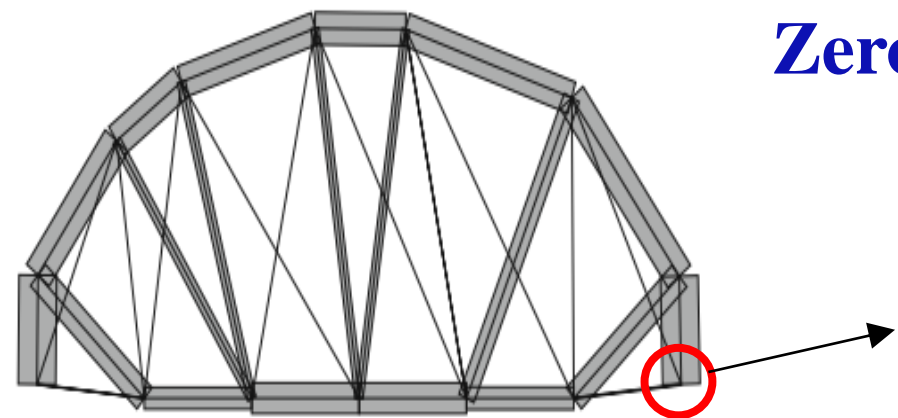
Source: Ohsaki M, Hayashi K. Force density method for simultaneous optimization of geometry and topology of trusses. Struct Multidiscip Optim, 2017

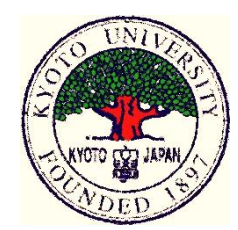


# Numerical Example 2



**Non-zero force element**





# *Conclusion*

---

## ➤ **Brief Summary**

**The proposed method includes :**

- **Shape and topology optimization**
- **Force density method**
- **Further optimization (Filter)**

**And has the following conclusion:**

- **Melting nodes can be avoid by restricting  $q$**
- **Stable optimal result can be obtained by using beam element**

*Thanks for your kind attention*



京都大学  
KYOTO UNIVERSITY

**Date : 2019.05.21**  
**Reporter : Wei Shen**